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DEVELOPMENT OF CARBON DIOXIDE (CO₂) SENSOR USING POLYMER NANOPARTICLES FOR GRAIN QUALITY MONITORING

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ABSTRACT A carbon dioxide sensor was developed using polyaniline boronic acid (PABA) conducting polymer nanoparticles as the electrically conductive region of the sensor and was demonstrated for use in detecting incipient or ongoing spoilage in stored grain. The developed sensor dynamically detected up to 2455 ppm of CO₂ concentration levels. The developed sensor was evaluated for the influence of temperature and relative humidity. The sensor's response to changes in the gas concentrations at various humidity and temperature levels was stable indicating that the sensor can dynamically detect CO₂ under fluctuating environmental conditions. The response of the PABA film to CO₂ concentration was not affected by the presence of alcohols and ketones, proving that the developed sensor is not cross-sensitive to these compounds which may be present in spoiling grain. The sensor packaging components were selected and built in such a way to avoid contamination of the sensing material and the substrate by undesirable components including grain dust and chaff. The developed conducting polymer CO₂ sensor exhibited dynamic performance in its response, recovery times, sensitivity, selectivity, stability and response slope when exposed to various carbon dioxide levels inside simulated grain bulk conditions.

Keywords: Carbon dioxide, polymer sensor, grain quality monitoring, nanosensor

INTRODUCTION The world annual grain production is about 2 Gt (billion metric tonnes) (USDA, 2007). Stored grain bulks are ecological systems where communities of insects, mites and microflora interact with abiotic variables to cause spoilage (Wallace & Sinha, 1981). While the importance of proper grain storage has been realized, post-harvest losses continue to range from 9% in North America to 50% in developing countries (FAO, 2000). Any loss in quality or quantity of the produced grain has far-reaching economic effects.

During the spoilage of grain, CO₂, moisture and heat are produced by the metabolism of the grain, fungi, insects and mites, and distinct odours are released. Increased levels of CO₂ in a stored grain bulk indicate that insects, mould, or excessive respiration are present. Evolution of excessive CO₂ from a stored grain mass is a reliable indicator of deteriorating grain. Carbon dioxide is also used as a fumigant for insect control during grain storage. During fumigation, there is a need to measure the CO₂ concentration throughout the grain mass to ensure uniform distribution and maintenance of CO₂ concentration. Intergranular air temperature and air composition will help to identify the location of spoilage inside the grain bulk.

Instruments capable of sensing CO₂ concentrations of 0.1% (atmospheric levels are 0.038%) will detect spoilage during stored grain in 80% of deteriorating bulks in farm granaries (Muir et al., 1985). Simulation models of Singh (Jayas) et al. (1983) and experimental data of Muir et al. (1985) concluded that in the absence of prior knowledge of the location of potential deterioration of grain, a sensor capable of detecting CO₂ levels of 2 g/m³ should be located near the centre of the bin. Ileleji et al. (2006) employed commercial CO₂ sensors near the vents and exhaust air stream of fans in the grain bin for measuring CO₂. They concluded that hot spot and early spoilage of grain can be detected inside grain bins using CO₂ sensors. Measurement of the intergranular CO₂ inside grain bulk remains a challenging task, mainly because of lack of availability of sensors and deployment issues.

The correlation between different ppm levels of CO₂ and indication of infestation in grain stores has been established by Semple et al. (1988) (Table 1). Most commercially available microfabricated sensors (e.g., Cole-Palmer, Chicago, USA; Figaro Engineering Inc., Osaka, Japan) are made of a substrate heated by wire and coated with a metal oxide, semiconducting film. The sensors cannot function without small heaters (usually platinum or gold) on the back side to keep the sensors at operating temperatures of 200 to 450°C. Because of the high operating temperatures, metal oxide sensors are inappropriate in potentially flammable environments (Dickinson et al., 1998) or explosive environment such as grain stores. Metal oxide based gas sensors are not recommended to monitor quality of food because irreversible binding of sulphur compounds may cause poisoning (Schaller et al., 1998).

Table 1. Carbon dioxide concentrations as an index of infestation in grain stores. Source: Semple et al. (1988).

CO ₂ Concentration	Indication of Infestation
380 to 500	Atmospheric concentration (no spoilage)
<1100	Incipient spoilage
1100 to 3500	Slight insect infestation and (or) infestation of microorganisms
3500 to 5000	High insect infestation and (or) a higher infection of microorganisms
5000 to 9000	Highly unsuitable storage conditions
>10000	Dangerous and extremely unsuitable storage conditions

With the advent of novel polymer materials and micro-nanotechnology, CO₂ micro-sensors can be fabricated and deployed inside grain bulk to measure the intergranular air composition. Polymer films are multifunctional, useful, economical, and practical in a

wide range of applications and sensor designs. Miniaturization of microelectronics favors the use of polymer thin films in sensors. The polyaniline boronic acid (PABA) has been used as a promising sensing material for developing a saccharide sensor (Shoji & Freund, 2002); a conductometric sensor for dopamine detection (Fabre & Taillebois, 2003); and an amine vapour detection sensor (English et al., 2006). The electrochemical potential of the polymer PABA is sensitive to changes in the pKa (acid dissociation constant) of the polymer as a result of its interaction with change in analyte concentrations (Shoji and Freund, 2002). The pH-dependent equilibria of PABA and its similarity in sensitivity to pH changes as that of polyaniline has been studied by Deore et al. (2006) and Deore & Freund (2009). The added advantages of using PABA as a sensing material for CO₂ detection are: the ability to be used as a simple physical dispersion process for electrode deposition, high environmental stability, and its water solubility during electro-chemical polymerization.

The objectives of this study were to: 1) develop and characterize a prototype CO₂ sensor using PABA, nafion electrolyte and selective gas permeable membranes; 2) evaluate the developed sensor for the effects of temperatures, relative humidity, and presence of selected chemical compounds; and 3) test prototype sensor for measuring varying gaseous CO₂ concentrations in simulated grain bulks.

EXPERIMENTALS

Gas flow management system A proper gas flow management system is crucial for successful sensor characterization. The gas flow management and the sensor evaluation system consists of a flow system to control the desired gas flow rates to the Teflon testing chamber, and a data collection system to record data from the sensor. Based on our design and input, an automated vapor delivery system was custom built by Plasmionique Inc., St Hyacinthe, PQ, Canada to control the flow rate of carbon dioxide and nitrogen gas using mass flow controllers and solenoid valves for delivering the known concentration of CO₂ to a Teflon gas mixing chamber and then to the sensor-testing chamber. This system allowed producing mixtures of analyte at various flow rates and at desired concentrations of analyte solutions. Commercially available gas cylinders (Praxair, Edmonton, AB) with a blend of CO₂/air mixture of 9820 ppm concentration and a nitrogen cylinder of ultra-high purity (99.99%) were used for the measurements. To achieve the required ppm levels of CO₂ concentrations, gas from 9820 ppm level was diluted to appropriate concentrations by mixing and varying the gas flow rate from the nitrogen cylinder.

Data collection system The data collection system used for characterization of the CO₂ sensor consists of an Agilent 34980A Data Acquisition Switch Unit (Agilent Technologies, Inc., Santa Clara, CA). The dc resistance of the sensor was read sequentially by the Agilent data acquisition unit. The control computer was interfaced with data collection system through an IEEE general purpose interface board (GPIB). The resistance data were initially stored in the data acquisition unit and once a complete set of data were recorded, the GPIB communications protocol sent the data to the control computer where the data were stored in a tab-limited text file. The gas flow management system and the data collection system were interlinked and connected through a LabVIEW (National Instruments Corporation, Austin, TX) algorithm to efficiently

control and simultaneously record the gas mixture readings and the sensor response output values.

Materials The reagents, chemicals and adhesives including 3-aminophenylboronic acid, poly aniline, phosphoric acid, sodium fluoride, ammonium persulfate, poly vinyl alcohol, potassium chloride, nafion, cyanoacrylate (Permabond 105), poly vinyl chloride, used for the sensor construction were of analytical grade and purchased from Sigma-Aldrich Inc (St. Louis, MO). All aqueous and buffer solutions were prepared with 18.2 M quality deionized water using an ultrapure water system (Millipore Corporation, Billerica, MA). Carbon dioxide porous PTFE membranes with 60 μm thickness and with average pore diameter of 0.2 μm were acquired from Thermo Scientific (Waltham, MA). Chemically resistant perfluoroelastomer O-rings of 0.3 mm diameter and 0.1 mm wall thickness used for mounting the PTFE gas permeable membrane were purchased from Fisher Scientific (Pittsburgh, PA).

PABA film synthesis Poly(anilineboronic acid)/phosphate nanoparticle dispersions were produced using the reactivity of the boronic acid moiety with phosphate in the presence of fluoride (Deore and Freund, 2009). The PABA dispersion solution was synthesized chemically using 10 mM 3-APBA (monomer) + 50 mM NaF + 5 mM ammonium persulfate (oxidant) in 0.1 M phosphoric acid. The chemical synthesis of PABA polymer is easily water dispersible, and hence it facilitated to form smooth, adherent and uniform thin films on the electrode surface. The PABA nanoparticles were in the range of 25-50 nm diameters. The dispersion of PABA nanostructures prepared in 0.1 M phosphoric acid with a concentration of 5 mg/mL was used as the sensing material of the sensor.

Sensor construction A cross-sectional side view of the constructed sensor assembly is shown in Fig. 1(A). Gold interdigitated array electrodes (IDAs) to be used as the sensor substrate platform, deposited on a 1 mm thick printed circuit board (PCB) was custom designed upon consultation with Iders Inc, Winnipeg, MB. The sensor chip was fabricated by Dynamic & Proto Circuits Inc, Stoney Creek, ON. Each sensor chip has seven sensor elements (detectors) (Figure 1(B)). A 2 μL PABA solution was deposited on the IDAs through a micropipette as a physical dispersion process and was allowed to dry for 20 min.

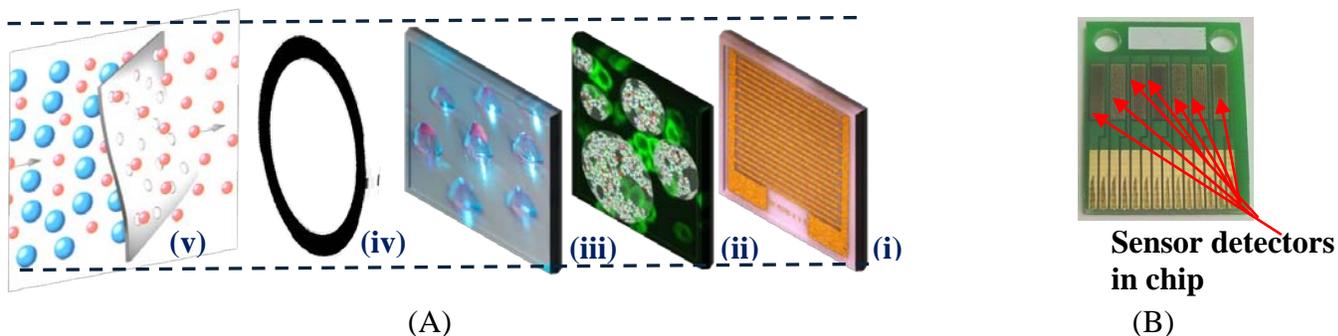
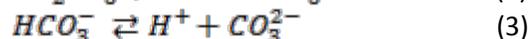
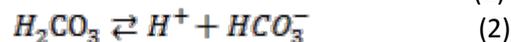
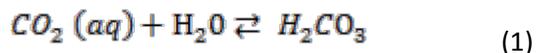


Figure 1 (A) Pictorial cross-sectional view of the CO₂ sensor (i) Gold interdigitated electrode PCB array, (ii) PABA polymer nanoparticles, (iii) Nafion, (iv) O-ring, (v) Gas permeable membrane. (B)

A 2 μL of Nafion solution was superimposed directly on top of the PABA thin film in the electrically conductive region of the sensor. The solution was then allowed to evaporate in air at 25°C and a dried residue was left to form the conductive sensing material. The polytetrafluoroethylene (PTFE) CO₂ selective gas permeable membrane (Sterlitetech Corporation, WA) was applied directly on top of the dried residue of the Nafion electrolyte with the aid of an O-ring. The membrane was cut into circular shapes of approximately 11 mm diameter and was attached to the O-rings by applying small amounts of cyanoacrylate adhesive. The O-ring with the mounted membranes was glued carefully to the PCB substrate of the sensor assembly, forming a cavity with the electrolyte/hydrogel composite and the PABA thin film below the membrane. Care was taken to apply the adhesive only on the rim of the O-ring and thereby avoiding the adhesive contact with the sensing material. The gap between the gas permeable membrane and the surface of the electrolyte/hydrogel composite was kept at a minimum distance (<0.2 mm) using an O-ring to maintain the thin layers of the electrolyte and sensing material.

RESULTS AND DISCUSSION

Sensor principle The sensing mechanism is based on the interconversion between conducting emeraldine salt form and the insulating emeraldine base form of polyaniline and PABA through protonation and deprotonation. When the analyte (gaseous CO₂) permeates through the gas permeable membrane, CO₂ reacts with water from nafion electrolyte to create a bicarbonate ion (HCO₃⁻) and a proton, which protonates the polyaniline. When the CO₂ diffuses through the gas-permeable membrane, the following equilibria are sequentially established (Jensen and Rechnitz, 1979).



As the CO₂ partial pressure increases, the conductivity increases due to increase in the amount of protonation. This changes the pH of the internal electrolyte. The potential changes linearly with the pH and thereby the concentration of the analyte can be measured. The potential of the electrode depends on the activities of hydronium ions. Nernst equation (Eq 4) relates the potential of electrochemical cell (or sensing assembly) as a function of concentration of ions in the reaction.

$$E = E_0 - \frac{RT}{nF} \ln(Q) \quad (4)$$

where Q is reaction coefficient and n is the number of electrons exchanged. Nernst equation accurately predicts cell potentials when the equilibrium quotient Q is expressed in ionic activities. The sensors were placed in the Teflon test chamber and were exposed, alternately, to clean dry background air and air containing analyte. The sensor exposures alternated between 5 min of clean background air and 5 min of different analyte concentrations for each analyte concentration. Baseline resistance for each sensor was established by flowing background air (air containing 380 ppm of CO₂) and at 0% humidity prior to various nitrogen and CO₂ exposure levels. Sensor data were recorded as

resistance versus time and the events such as an exposure to various CO₂ levels or a change in humidity or temperature were analyzed as normalized changes in resistance ($\Delta R_m/R_b$).

$$\frac{\Delta R_m}{R_m} = \frac{(R_m - R_b)}{R_b} \quad (5)$$

R_m = sensor resistance at the plateau of the response

R_b = resistance prior to the event

The data was processed using background determination as R_b prior to an exposure of analyte to correct for baseline drift.

Effect of humidity For functional feasibility, the sensor industry prefers solid electrolyte over liquid electrolyte to maintain compactness of sensor cells considering the size of packaging components, leakage, and drying up of liquid electrolyte under high humidity/temperature conditions. Nafion has been widely used as a proton exchange membrane in polymer electrode fuel cell applications. The results of the relationship between resistance and CO₂ concentration for the PABA-Nafion sensor under various humidity (RH) levels are shown in Figure 2. It has been reported (Skotheim et al., 1998) that the conductivity of conducting polymers increases when the film absorbs the moisture. The resistance value of PABA decreased with humidity level due to the possibility of proton exchange between the water molecules and the protonated and the unprotonated forms of PABA.

PABA-Nafion sensor showed two step sensing response to humidity levels. The resistance value of the sensor electrodes decreased when RH increased from 20 to 50% indicating that the water molecules might have been absorbed by the PABA film. The charge transfer process of conducting species with water molecules resulted into the decrease in the resistance value. The resistance values of the sensor increased when RH increased from 50% to 70%. The mechanism of charge transfer process may be different for the humidity levels between 50 to 70% RH. The deviation in the linearity could be attributed to the size of the pores of polymer. Similar deviation in the linearity behaviour was observed by Parvatikar et al. (2006) in a Polyaniline/tungsten oxide composite sensor when exposed to humidity levels between 20 to 90% RH. In the characterization of PANI/tungsten composite, the resistance is found to drop down from 20 to 50% RH in a linear fashion while, after 60% RH, saturation is observed with a very small decrease in the resistance up to 90% RH. They speculated that between 20 to 50% RH level, the hole concentration is increased by donation of the lone pair from the conducting complex towards the tungsten oxide water molecules. Thus, the partial charge transfer process of conducting species with that of water molecules resulted in the decreased sheet resistivity. For higher humidity levels above 50% RH, the mechanism may be different leading to two step response of the sensor.

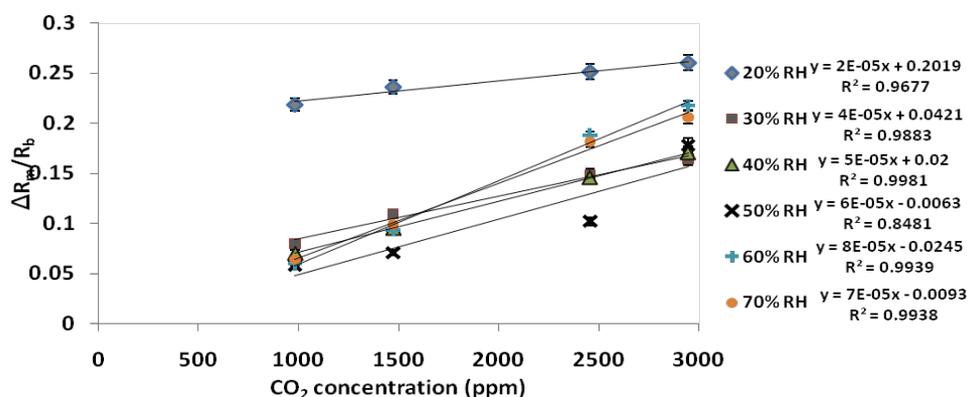


Figure 2. Variation of resistance with change in relative humidity (%) for PABA-Nafion sensor at 25°C.

As the humidity increases from 20% to 50% RH, there may be more hydrogen carbonate ions and protons produced on the PABA film, thus lowering the resistance of the film. The polymer might swell due to water absorption and there may be breakdown or increase in contact between the dispersed conductive nanoparticles affecting the resistance value with the change in humidity. Above 50% RH level, the pores might be saturated causing a change in diffusion pathways. The variation in the resistance parameter was curvi-linear and repeatable. The film's response to change in analyte concentrations at various humidity levels was very stable until 70% RH and becomes noisy above 70% RH. At humidity levels above 70% RH, the sensors might still perform well when provided with a rugged membrane protection and a proper sensor packaging. Irrespective of the change in resistance values at different humidity levels, all the PABA-Nafion sensors responded to various levels of CO₂ concentrations up to 2455 ppm.

The sensor electrodes displayed a saturation effect above 2455 ppm of CO₂. The sensor's working principle depends on the extraction of ions due to the change in protonation state from the PABA film. Changing the morphology of films by creating a higher surface area through nanorods or nanofiber structures in the polyaniline film might enhance the sensitivity and response time of the sensor (Virji et al., 2004). Future research is required to explore the possibility of enhancing the response time and sensitivity of PABA thin film by varying morphology. The larger the porous structure of the PABA thin film, the larger will be the reaction surface and inner space for the electrolyte penetration into the film. So, this might shorten the diffusion pathways for the counter ions leading to quicker response time.

Effect of temperature The influence of temperature on the performance of the constructed sensors was evaluated by allowing the analyte gas to pass through a copper coil immersed in heated water bath circulator (Model 12108-20 Cole-Parmer Instrument Company, Vernon Hills, IL). The temperature range was maintained from 25°C to 55°C. The sensor chip was also tested at various CO₂ levels after storing the chip at -25°C for 48 h and then at the room temperature for about 2 h before placing it in the testing chamber at 25°C. The temperature of the analyte gas inside the testing chamber was monitored using a temperature sensor (Model 44034 Omega Precision Thermistor, Omega Engineering Inc, Stamford, CT).

For the PABA-Nafion sensor, the resistance value decreased from 6000 to 1044 ohms when the temperature increased from 25°C to 55°C when exposed to 2400 ppm CO₂. Experiments were conducted by changing the order of heating the CO₂ gas flow and similar trend was observed indicating that the phenomenon is reversible irrespective of the temperature order. The decrease in the resistance value upon increase in temperature (Figure 3) may be due to the loss of protonation and expulsion of water molecules from the polymer composite. In terms of thermal stability, the influence of the acid used for the protonation of PANI is more than the polyaniline backbone itself, because polyaniline has the ability to sustain exposure to an elevated temperature of 173°C without decisive damage (Prokes and Stejskal, 2004). The increase in resistance value with exposure to -25°C may be explained by the change in the morphology of the film and the restriction of the transportation of charge carriers.

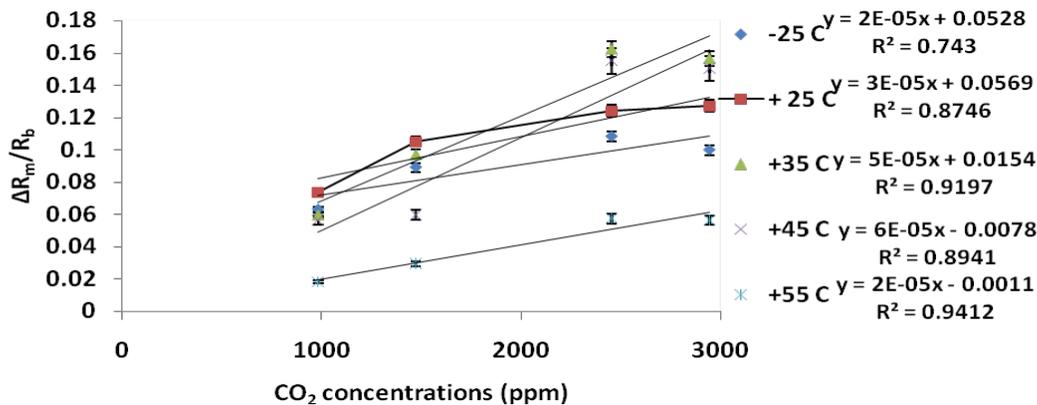


Figure 3. Variation of resistance with change in temperature (°C) for PABA-Nafion sensor at 50% RH level.

The sensor did not respond to various CO₂ concentrations and the response became noisy above 55°C. To assess the influence of temperature, experiments were conducted at 50% RH for measurements at 25°C. As the temperature increased from 25 to 55°C, the water molecules in the air might be reduced to a greater extent.

Repeatability and reproducibility Sensor repeatability refers to the successive runs made using a single sensor to evaluate discrepancies in its response. Sensor reproducibility refers to the sensor variations in response between individual chips of a batch of similarly constructed sensors. The repeatability of the sensor was studied by using the same sensor to repeatedly (five times) measure the response to different CO₂ concentrations (Figure 4). At the same time, the reproducibility of the sensor was studied by using five similarly constructed sensors to measure the response at various CO₂ gas levels (Figure 5). In the reproducibility study, the same response trend was observed for all of the sensors on the same chip. Each sensor chip has seven sensors and the response of the sensors is shown in Figure. 4. The response of the sensors was not stabilized initially and over the course of time (5 min), it became stabilized. The relative standard deviation for reproducibility of the sensor was 11%. Variation in the response of the sensor could be due to the construction variation and operational variation. The sensitivity got better with time/exposure as trial 4 and trial 5 responses are nearly

overlapping. The same trend was observed for all sensor electrodes in different chips (data not shown).

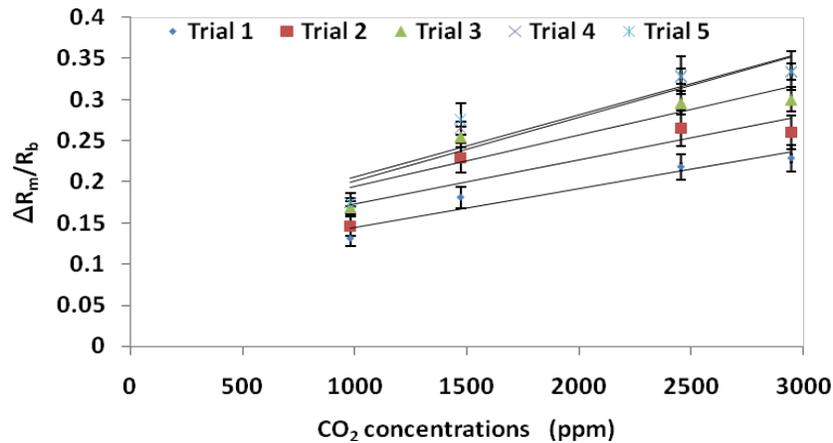


Figure 4. Response of PABA-Nafion Sensor Chip #64 (5 trials, same electrode) to various concentrations of CO₂ at 40% RH and at 25° C.

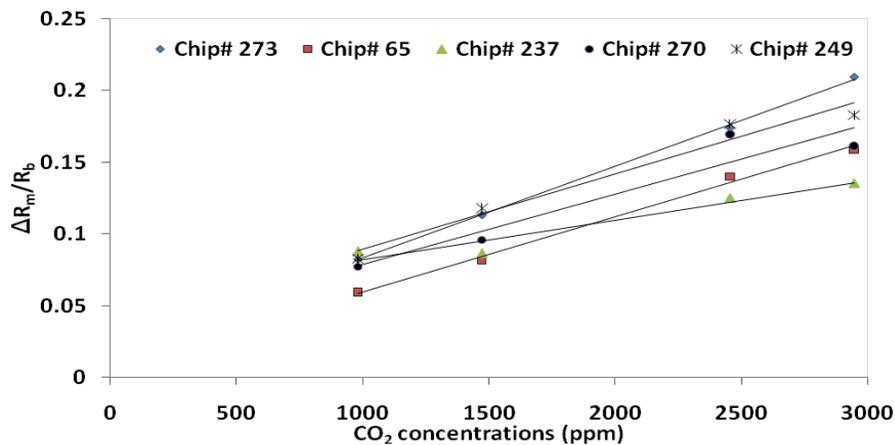


Figure 5. Response of 5 different similarly constructed PABA-Nafion sensors to various concentrations of CO₂ at 40% RH and at 25° C.

Dynamic characteristics Sensitivity, linearity, accuracy, drift and hysteresis properties have transient effects that are settled to their steady state and are the static characteristics of a sensor. The experimental results on the effect of humidity and temperature indicate that the response of the PABA-Nafion sensor to various levels of CO₂ is linear up to 2455 ppm and above that a saturation effect is observed. Prior to actual measurements, the sensor was exposed for 20 min in the background gas flow to achieve stabilized response and to reduce associated drift. The repeatability and reproducibility experiments results show that the PABA-Nafion sensor is accurate with higher sensitivity. A sensor's sensitivity indicates how much the sensor's output changes upon exposure to analyte. Drying the sensor electrodes after material deposition over 30 min reduced the drift to a large extent. The dynamic characteristics of a sensor are determined by analyzing the response of the sensor to variable input of analyte (CO₂) concentrations such as step mode, ramp mode (Figure 6) and random measurement (data not shown).

Characterization of the PABA-Nafion sensor's dynamic response was evaluated by comparing the step mode and ramp mode measurement. The ramp mode response curve shows that the PABA-Nafion sensors did not respond to CO₂ levels above 2455 ppm. The step or pulsed mode measurement shows that the response curve was reversible upon exposure to background gas.

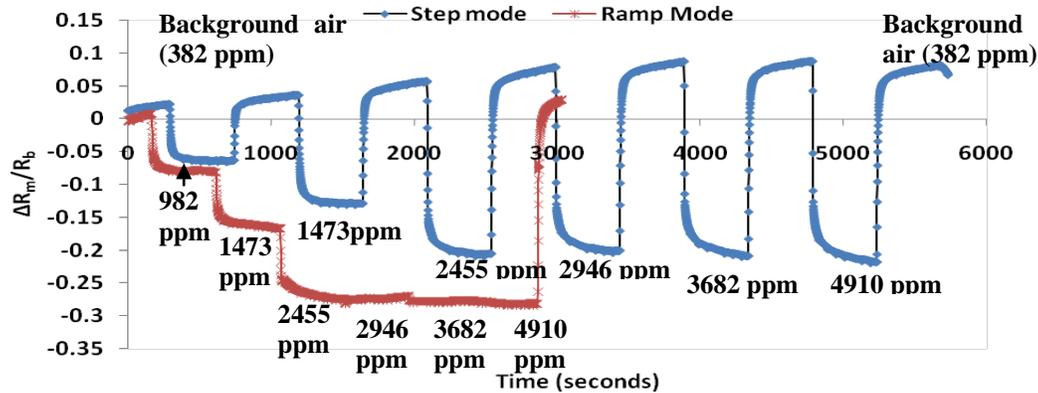


Figure 6. Response of the PABA-Nafion sensor operated in step and ramp mode to various concentrations of CO₂ and subsequent exposure to background air at 40% RH and at 25°C.

Evaluation of gas permeable membrane / Cross Sensitivity By selecting appropriate gas permeable membranes with different pore size and thickness, the sensitivity and (or) the linear range of the sensor can be optimized to certain extent. The membranes act as a protecting cover for the electrolyte and the sensing material in the sensing reservoir on the electrode arrays. The PTFE membrane is highly selective to CO₂ and does not allow other gas molecules to pass through hence aiding in reducing the cross-sensitivity effect of the sensor (data not shown). For efficient functioning of sensors, there is a need to find out whether the sensor is interfered by other gases in addition to target analyte gas. The dc resistance values decreased with increasing CO₂ concentration indicating an increase of conductivity due to CO₂ concentration levels. But upon random exposure of 1% (percent of vapour pressure) of methanol (1618 ppm), acetone (3157 ppm) and 1-propanol (276 ppm) (representative of compounds expected in stored grain (Loschiavo et al., 1986; Borjesson et al., 1989)) in air for 3 min, followed by various levels of CO₂ did not change the resistivity of the sensor. The PABA-Nafion sensor works on the principle of pH change and CO₂ being acidic reacts with the electrolyte to induce ionic exchange resulting in decreased resistivity. The gas permeable membrane is selective to CO₂ and allows only CO₂ molecules to pass through. Hence there was no response (Figure 7) due to alcohols and ketones in air.

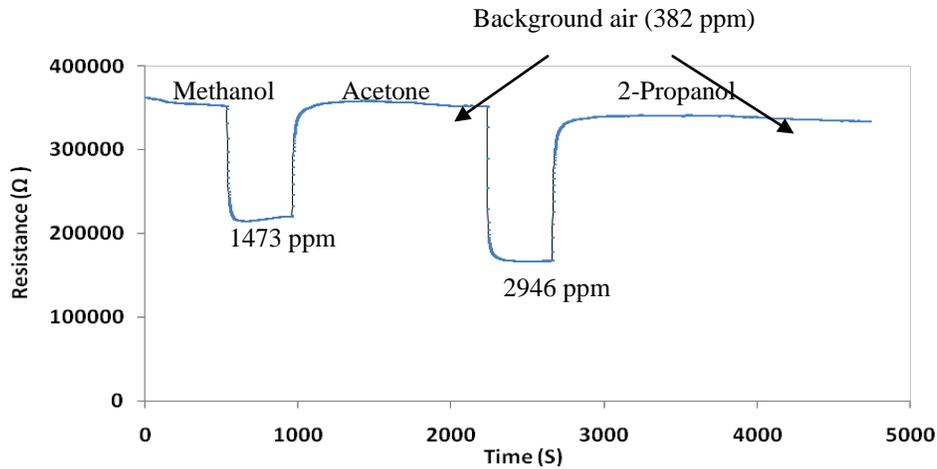


Figure 7. Response of the PABA sensor with selective gas permeable PTFE membrane to CO₂, methanol, acetone and 2-propanol analytes of 1% in air at 40% RH and at 25°C.

Sensor packaging Miniature sensor elements will usually not function on their own. The sensor packaging (Figure 8) gives the sensor a suitable shape or form, provides electrical connection to the sensor, and provides a window from the sensor to the outside world. In addition, the sensor elements need mechanical and chemical protection. To package the CO₂ sensor for preliminary testing in bulk grain several options were considered to ensure that the packaging components avoid contamination of the sensing material and the substrate by undesirable components including grain dust and foreign material in grain. The dimensional details of the sensor chip and gas diffusion properties of the packaging material were considered in selecting the packaging components. The performance characteristics of the sensors depend on the geometry of electrodes, thermal design of the structure and the nature of the electronic interface.

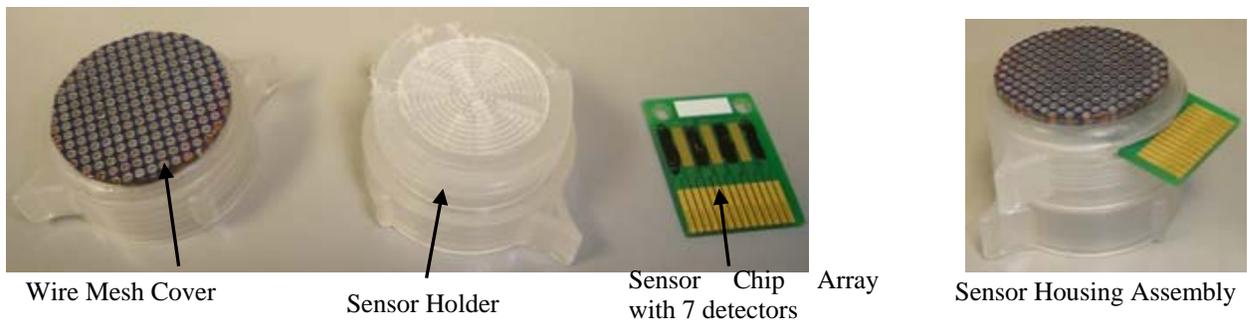


Figure 8. Picture of the Sensor Housing Assembly Packaging

Sensor's performance inside simulated grain bulk The CO₂ sensor packaged in the prototype housing assembly (Figure 9) was tested in plastic pails (4 L capacity) filled with wheat. The pails were purged with known CO₂ concentrations to simulate spoilage of grain. The sensor exhibited excellent response (Fig. 16) to change in CO₂ levels inside grain bulk. The CO₂ gas at desired levels was passed through the bottom of the pail while the sensor was kept immersed in the grain bulk at the top. The plastic pail was covered tightly with duct tape to prevent atmospheric exchange into the grain bulk. Gas

samples from the outlet tube were analyzed using GC-MS to determine the concentrations of the outlet gas.

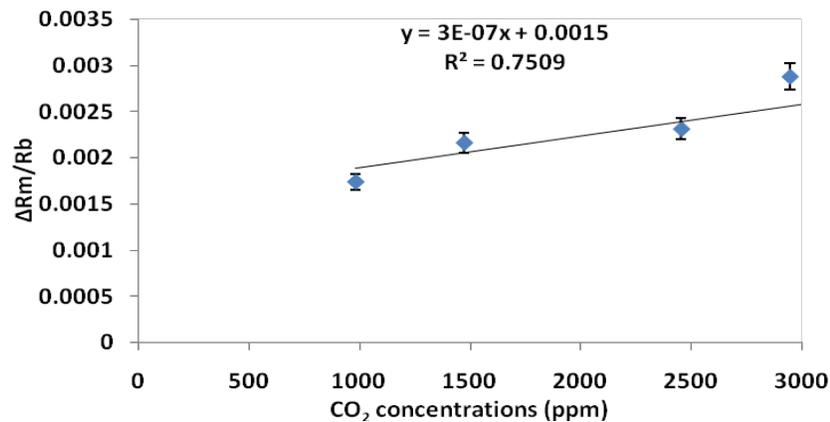


Figure 9. Response of PABA Nafion Sensor with packaging kept inside grain bulk to concentrations of CO₂ at 50% RH and at 25°C.

CONCLUSION A sensitive tool for detecting incipient or ongoing deterioration of stored grains by measuring CO₂ levels was developed using PABA conducting polymer nanoparticles. The developed CO₂ sensor can monitor the CO₂ concentration in stored grain bulks, permitting the detection of CO₂ between 20 to 70% equilibrium relative humidity. The sensor dynamically detected up to 2455 ppm of CO₂ levels in the grain bulk. The CO₂ sensor exhibited dynamic performance in its response, recovery time, sensitivity, selectivity, stability and response slope. The CO₂ sensor responded well to various concentrations of CO₂ at temperatures between 25°C to 55°C. The sensors respond to various levels of CO₂ at ambient temperature without artificial cooling. The packaging unit allowed measurement of CO₂ concentration efficiently inside the grain bulk. The methodology used for building the CO₂ sensor device is compatible with the MEMS process (printed circuit board process) and can be mass manufactured using screen printing technology.

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